

Title:

ENDF/B-V AND ENDF/B-VI RESULTS FOR UO-2 LATTICE BENCHMARK PROBLEMS USING MCNP

CONF-981003--

Author(s):

R. D. Mosteller

RECEIVED

MAY 28 1998

OSTI

Submitted to:

Int'l Conf. on Physics of Nuclear Science & Technology, Islandia, Long Island, NY  
October 5-8, 1998

MASTER

DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED *ph*

**Los Alamos**  
NATIONAL LABORATORY

Los Alamos National Laboratory, an affirmative action/equal opportunity employer, is operated by the University of California for the U.S. Department of Energy under contract W-7405-ENG-36. By acceptance of this article, the publisher recognizes that the U.S. Government retains a nonexclusive, royalty-free license to publish or reproduce the published form of this contribution, or to allow others to do so, for U.S. Government purposes. The Los Alamos National Laboratory requests that the publisher identify this article as work performed under the auspices of the U.S. Department of Energy.

## DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

## **DISCLAIMER**

**Portions of this document may be illegible in electronic image products. Images are produced from the best available original document.**

**ENDF/B-V AND ENDF/B-VI RESULTS FOR  
UO<sub>2</sub> LATTICE BENCHMARK PROBLEMS  
USING MCNP**

Russell D. Mosteller

Advanced Nuclear Technology Group  
Nonproliferation and International Security Division  
Los Alamos National Laboratory

To Be Submitted for Presentation at the  
International Conference on the Physics of Nuclear Science and Technology

Islandia, Long Island, NY

October 5-8, 1998

## ENDF/B-V AND ENDF/B-VI RESULTS FOR UO<sub>2</sub> LATTICE BENCHMARK PROBLEMS USING MCNP

Calculations for the ANS UO<sub>2</sub> lattice benchmark<sup>1</sup> have been performed with the MCNP Monte Carlo code<sup>2</sup> and its ENDF/B-V and ENDF/B-VI continuous-energy libraries. Similar calculations were performed previously<sup>3</sup> for the experiments upon which these benchmarks are based, using continuous-energy libraries derived from ENDF/B-V and from Release 2 of ENDF/B-VI (ENDF/B-VI.2). This study extends those calculations to the infinite-lattice configurations given in the benchmark specifications and also includes results from Release 3 of ENDF/B-VI (ENDF/B-VI.3) for both the core and infinite-lattice configurations.

For this set of benchmarks, the only significant difference between the ENDF/B-VI.2 and ENDF/B-VI.3 libraries is the cross-section behavior of <sup>235</sup>U. ENDF/B-VI.3 contains revised cross sections for <sup>235</sup>U below 900 eV,<sup>4</sup> although those changes principally affect the range below 110 eV.<sup>5,6</sup> In particular, relative to ENDF/B-VI.2, ENDF/B-VI.3 increases the epithermal capture-to-fission ratio for <sup>235</sup>U and slightly increases its thermal fission cross section.

Each MCNP case discussed herein was run with 4,000 particles per generation and 1,050 generations. The first 50 generations were excluded from the statistics, thereby producing 4,000,000 active histories for each case.

The values for  $k_{\text{eff}}$  for the core problems are reported in Table 1, along with the resulting differences from the benchmark value ( $1.0007 \pm 0.0006$ ). The corresponding pin power distributions in the central assembly are shown in Figures 1 and 2.

ENDF/B-V appears to underpredict  $k_{\text{eff}}$  slightly for these cases. However, it has been reported<sup>7</sup> that deficiencies in the MCNP ENDF/B-V library for <sup>238</sup>U produce a bias of approximately  $-.003 \Delta k$  in the calculated value of  $k_{\text{eff}}$  for thermal lattices with low-enriched UO<sub>2</sub> fuel. If that bias is applied to these results, ENDF/B-V produces excellent agreement with the benchmark value for  $k_{\text{eff}}$ : all three values for  $k_{\text{eff}}$  are within 2 standard deviations of the benchmark value, and the difference between the benchmark and calculated means is  $0.0012 \Delta k$  or less.

The ENDF/B-VI results for  $k_{\text{eff}}$  are not as good as those from ENDF/B-V. The calculated values of  $k_{\text{eff}}$  are approximately half a percent too low, with the ENDF/B-VI.3 value slightly but consistently lower than the ENDF/B-VI.2 value.

The pin power distributions from the three libraries all are in good agreement with the measured values, with an RMS difference of approximately 2% between the measured and calculated sample means. The RMS differences between the calculated sample means are slightly smaller, ranging from 1.1% to 1.9%. However, it is likely that the size of these differences would decrease somewhat if additional Monte Carlo histories were run to reduce the calculated standard deviations.

The values for  $k_{\text{eff}}$  and the various spectral indices from the infinite-lattice calculations are reported in Table 2, and the corresponding pin power distributions are shown in Figures 3 and 4. Not surprisingly, the results from the infinite-lattice cases produce patterns that are similar to those observed for the core cases. For example, the RMS differences between the pin power distributions for the infinite-lattices cases are only 0.3% to 0.4%, which is comparable to the standard deviations in the pin powers. These results, in conjunction with those for the core problems, strongly suggest that all three libraries produce essentially the same power distributions for these benchmarks.

Nonetheless, there are subtle changes to the reactivity differences that reflect cross section differences between the libraries. In particular, the reactivity differences between the ENDF/B-V and ENDF/B-VI results decrease slightly relative to the core cases, which suggests that leakage from the core to the reflector is slightly higher for the ENDF/B-VI cases. Such behavior is consistent with differences in the ENDF/B-V and ENDF/B-VI cross sections for  $^{16}\text{O}$  at high energies.

Differences in the spectral indices also reflect cross section differences between the libraries and thereby help to explain the observed reactivity differences. The values for  $\rho_{25}$  are consistent with the epithermal  $^{235}\text{U}$  capture-to-fission ratio in the three libraries (i.e.,  $\rho_{25}$  is lowest for ENDF/B-VI.2 and highest for ENDF/B-VI.3). The results from both ENDF/B-VI libraries for  $\rho_{28}$  and for the conversion ratio are higher than those from ENDF/B-V, and such behavior indicates higher neutron capture rates in  $^{238}\text{U}$  (the ENDF/B-VI.3 values are slightly but consistently lower than their ENDF/B-VI.2 counterparts, reflecting the increased competition between  $^{235}\text{U}$  and  $^{238}\text{U}$  in the epithermal region). All three libraries produce essentially the same values for  $\delta_{28}$  but the ENDF/B-VI values for  $\delta_{25}$  are lower than those from the ENDF/B-V calculations. This combination suggests that reactivity differences between ENDF/B-VI and ENDF/B-V are due, at least in part, to increased fast capture in  $^{238}\text{U}$  and decreased fast fission in  $^{235}\text{U}$ .

Overall, ENDF/B-V produces significantly better agreement with the benchmark values for  $k_{\text{eff}}$  than do either of the ENDF/B-VI libraries. The pin power distributions, however, are essentially the same irrespective of the library. Finally, the spectral indices from the infinite-lattice cases are consistent with the known cross section behavior in the three libraries and help to explain the observed reactivity differences.

## References

1. T. A. Parish, et al., "Summary of Results For the ANS Uranium Benchmark Problem," submitted for presentation at the International Conference on the Physics of Nuclear Science and Technology.
2. Judith A. Briesmeister, Ed., "MCNP—A General Monte Carlo N-Particle Transport Code, Version 4A," Los Alamos National Laboratory report LA-12625-M (November 1993).

3. Russell D. Mosteller, Stephanie C. Frankle, and Phillip G. Young, "Data Testing of ENDF/B-VI with MCNP: Critical Experiments, Thermal-Reactor Lattices, and Time-of-Flight Measurements," Jeffrey Lewins and Martin Becker, Eds., **Advances in Nuclear Science and Technology, Volume 24**, pp. 131-195, Plenum Press (1997).
4. C. R. Lubitz, "A Modification to ENDF/B-VI  $^{235}\text{U}$  to Increase Epithermal Alpha and  $K_1$ ," *Proceedings of the International Conference on Nuclear Data for Science and Technology*, CONF-940507 (May 1994).
5. A. C. Kahler, "Homogeneous Critical Monte Carlo Eigenvalue Calculations with Revised ENDF/B-VI Data Sets," *Trans. Am. Nucl. Soc.*, **72**, 384 (June 1995).
6. M. L. Williams, R. Q. Wright, and M. Asgari, "ENDF/B-VI Performance for Thermal Reactor Analysis," *Trans. Am. Nucl. Soc.*, **73**, 420 (October 1995).
7. F. Rahnema and H. N. M. Gheorghiu, "ENDF/B-VI Benchmark Calculations for the Doppler Coefficient of Reactivity," *Ann. Nucl. Energy*, **23**, No. 12, pp. 1011- 1019 (August 1996).

Table 1. MCNP Results for Core Configurations.

Core	$k_{\text{eff}}$			$\Delta k$		
	ENDF/B-V	ENDF/B-VI.2	ENDF/B-VI.3	ENDF/B-V	ENDF/B-VI.2	ENDF/B-VI.3
A	0.9981 ± 0.0003	0.9963 ± 0.0003	0.9956 ± 0.0003	-0.0026 ± 0.0007	-0.0044 ± 0.0007	-0.0051 ± 0.0007
B	0.9988 ± 0.0003	0.9964 ± 0.0003	0.9957 ± 0.0003	-0.0019 ± 0.0007	-0.0043 ± 0.0007	-0.0050 ± 0.0007
C	0.9965 ± 0.0003	0.9944 ± 0.0003	0.9940 ± 0.0003	-0.0042 ± 0.0007	-0.0063 ± 0.0007	-0.0067 ± 0.0007

Water Hole	1.107 ± 0.002	1.026 ± 0.006	1.000 ± 0.001	1.025 ± 0.007	1.026 ± 0.003	0.980 ± 0.021	0.983 ± 0.008
	1.122 ± 0.013	1.028 ± 0.012	1.014 ± 0.012	1.005 ± 0.012	1.002 ± 0.011	0.989 ± 0.011	0.963 ± 0.011
	1.124 ± 0.013	1.049 ± 0.012	1.025 ± 0.012	1.019 ± 0.012	1.040 ± 0.012	1.008 ± 0.011	0.966 ± 0.011
	1.119 ± 0.013	1.059 ± 0.012	1.017 ± 0.011	1.028 ± 0.012	1.021 ± 0.012	0.978 ± 0.011	0.963 ± 0.011
1.068 ± 0.002	1.075 ± 0.000	1.036 ± 0.007	1.047 ± 0.004	1.098 ± 0.006	1.026 ± 0.023	1.003 ± 0.031	
1.080 ± 0.012	1.096 ± 0.009	1.049 ± 0.009	1.045 ± 0.009	1.074 ± 0.009	1.018 ± 0.008	0.969 ± 0.008	
1.088 ± 0.012	1.117 ± 0.010	1.060 ± 0.009	1.048 ± 0.009	1.098 ± 0.009	1.026 ± 0.009	0.958 ± 0.008	
1.072 ± 0.012	1.107 ± 0.009	1.051 ± 0.009	1.047 ± 0.009	1.070 ± 0.009	1.013 ± 0.009	0.969 ± 0.008	
		Water Hole		Water Hole			
		1.116 ± 0.012	1.118 ± 0.011	1.133 ± 0.010	1.070 ± 0.010	1.070 ± 0.010	0.961 ± 0.010
		1.130 ± 0.009	1.137 ± 0.009	1.128 ± 0.009	1.083 ± 0.009	1.083 ± 0.009	0.979 ± 0.008
		1.139 ± 0.009	1.117 ± 0.009	1.123 ± 0.009	1.070 ± 0.009	1.070 ± 0.009	0.990 ± 0.008
		1.113 ± 0.009	1.139 ± 0.009	1.135 ± 0.009	1.073 ± 0.009	1.073 ± 0.009	0.984 ± 0.008
		1.091 ± 0.009	1.145 ± 0.008	1.133 ± 0.010	1.032 ± 0.026	1.032 ± 0.026	0.924 ± 0.006
		1.071 ± 0.012	1.152 ± 0.009	1.128 ± 0.009	1.019 ± 0.008	1.019 ± 0.008	0.987 ± 0.008
		1.101 ± 0.012	1.152 ± 0.009	1.123 ± 0.009	1.007 ± 0.008	1.007 ± 0.008	0.974 ± 0.008
		1.097 ± 0.012	1.148 ± 0.009	1.135 ± 0.009	1.030 ± 0.008	1.030 ± 0.008	0.972 ± 0.008
			Water Hole				
				1.109 ± 0.007	1.007 ± 0.014	1.007 ± 0.014	0.974 ± 0.026
				1.096 ± 0.009	1.008 ± 0.008	1.008 ± 0.008	0.961 ± 0.008
				1.087 ± 0.009	0.974 ± 0.008	0.974 ± 0.008	0.949 ± 0.008
				1.095 ± 0.009	1.003 ± 0.009	1.003 ± 0.009	0.953 ± 0.008
				1.015 ± 0.002	0.973 ± 0.023	0.973 ± 0.023	0.971 ± 0.012
				1.010 ± 0.011	0.980 ± 0.008	0.980 ± 0.008	0.955 ± 0.008
				1.006 ± 0.012	0.960 ± 0.008	0.960 ± 0.008	0.939 ± 0.008
				1.019 ± 0.012	0.976 ± 0.008	0.976 ± 0.008	0.944 ± 0.008
					0.970 ± 0.006	0.970 ± 0.006	0.950 ± 0.005
					0.960 ± 0.012	0.960 ± 0.012	0.931 ± 0.008
					0.952 ± 0.011	0.952 ± 0.011	0.934 ± 0.008
					0.932 ± 0.011	0.932 ± 0.011	0.937 ± 0.008
					Measured	Measured	0.920 ± 0.013
					ENDF/B-V	ENDF/B-V	0.919 ± 0.011
					ENDF/B-VI.2	ENDF/B-VI.2	0.934 ± 0.011
					ENDF/B-VI.3	ENDF/B-VI.3	0.934 ± 0.011

RMS Differences  
between Sample Means  
ENDF/B-V: 0.020  
ENDF/B-VI.2: 0.024  
ENDF/B-VI.3 0.019

Figure 1. Pin Power Distribution in Central Assembly of Core B.

Water Hole	1.148 ± 0.007	1.027 ± 0.004	1.045 ± 0.006	1.057 ± 0.006	1.047 ± 0.005	1.088 ± 0.004	1.124 ± 0.016
	1.152 ± 0.020	1.050 ± 0.017	1.039 ± 0.017	1.021 ± 0.016	1.066 ± 0.017	1.072 ± 0.017	1.124 ± 0.017
	1.175 ± 0.020	1.059 ± 0.017	1.050 ± 0.017	1.028 ± 0.016	1.035 ± 0.017	1.080 ± 0.017	1.118 ± 0.017
1.144 ± 0.019	1.048 ± 0.017	1.021 ± 0.016	1.034 ± 0.017	1.009 ± 0.016	1.106 ± 0.017	1.106 ± 0.017	1.114 ± 0.017
1.036 ± 0.005	0.945 ± 0.007	1.001 ± 0.006	0.982 ± 0.021	0.962 ± 0.008	1.070 ± 0.014	1.105 ± 0.009	1.105 ± 0.009
1.067 ± 0.018	0.939 ± 0.012	1.009 ± 0.012	0.997 ± 0.012	0.963 ± 0.011	1.060 ± 0.012	1.123 ± 0.013	1.123 ± 0.013
1.102 ± 0.018	0.965 ± 0.012	0.998 ± 0.012	0.991 ± 0.012	0.962 ± 0.012	1.063 ± 0.012	1.104 ± 0.013	1.104 ± 0.013
1.069 ± 0.018	0.957 ± 0.012	0.967 ± 0.012	0.985 ± 0.012	0.958 ± 0.012	1.050 ± 0.012	1.099 ± 0.009	1.099 ± 0.009
	Pyrex Rod	0.901 ± 0.006	0.900 ± 0.019	0.962 ± 0.008	1.001 ± 0.021	1.087 ± 0.007	1.087 ± 0.007
		0.908 ± 0.011	0.897 ± 0.011	0.990 ± 0.011	0.990 ± 0.011	1.094 ± 0.012	1.094 ± 0.012
		0.891 ± 0.011	0.900 ± 0.011	0.900 ± 0.011	1.004 ± 0.012	1.094 ± 0.012	1.094 ± 0.012
	0.902 ± 0.011	0.890 ± 0.011	0.900 ± 0.011	0.890 ± 0.011	1.005 ± 0.012	1.097 ± 0.012	1.097 ± 0.012
		0.914 ± 0.004	0.854 ± 0.017	0.933 ± 0.005	1.049 ± 0.014	1.088 ± 0.005	1.088 ± 0.005
		0.924 ± 0.016	0.866 ± 0.011	0.909 ± 0.011	1.035 ± 0.012	1.120 ± 0.012	1.120 ± 0.012
		0.927 ± 0.016	0.893 ± 0.011	0.915 ± 0.011	1.056 ± 0.012	1.094 ± 0.012	1.094 ± 0.012
		0.938 ± 0.016	0.878 ± 0.011	0.912 ± 0.011	1.033 ± 0.012	1.122 ± 0.012	1.122 ± 0.012
			Pyrex Rod	0.970 ± 0.006	1.097 ± 0.020	1.138 ± 0.015	1.138 ± 0.015
		0.950 ± 0.012		1.096 ± 0.012	1.149 ± 0.013	1.149 ± 0.013	1.149 ± 0.013
		0.959 ± 0.012		1.106 ± 0.012	1.135 ± 0.013	1.135 ± 0.013	1.135 ± 0.013
		0.954 ± 0.011	1.105 ± 0.012	1.105 ± 0.012	1.146 ± 0.013	1.146 ± 0.013	1.146 ± 0.013
		1.071 ± 0.006	1.140 ± 0.014	1.140 ± 0.014	1.195 ± 0.006	1.195 ± 0.006	1.195 ± 0.006
		1.050 ± 0.016	1.133 ± 0.013	1.133 ± 0.013	1.164 ± 0.013	1.164 ± 0.013	1.164 ± 0.013
		1.057 ± 0.016	1.135 ± 0.013	1.135 ± 0.013	1.144 ± 0.013	1.144 ± 0.013	1.144 ± 0.013
		1.087 ± 0.017	1.145 ± 0.013	1.145 ± 0.013	1.173 ± 0.013	1.173 ± 0.013	1.173 ± 0.013
		1.164 ± 0.003	1.164 ± 0.003	1.164 ± 0.003	1.199 ± 0.008	1.199 ± 0.008	1.199 ± 0.008
		1.150 ± 0.018	1.150 ± 0.018	1.150 ± 0.018	1.198 ± 0.013	1.198 ± 0.013	1.198 ± 0.013
		1.157 ± 0.017	1.157 ± 0.017	1.157 ± 0.017	1.171 ± 0.013	1.171 ± 0.013	1.171 ± 0.013
		1.181 ± 0.018	1.181 ± 0.018	1.181 ± 0.018	1.209 ± 0.013	1.209 ± 0.013	1.209 ± 0.013
		Measured	1.206 ± 0.011	1.206 ± 0.011	1.206 ± 0.011	1.206 ± 0.011	1.206 ± 0.011
		ENDF/B-V	1.244 ± 0.019	1.244 ± 0.019	1.244 ± 0.019	1.244 ± 0.019	1.244 ± 0.019
		ENDF/B-VI.2	1.215 ± 0.018	1.215 ± 0.018	1.215 ± 0.018	1.215 ± 0.018	1.215 ± 0.018
		ENDF/B-VI.3	1.238 ± 0.018	1.238 ± 0.018	1.238 ± 0.018	1.238 ± 0.018	1.238 ± 0.018

RMS Differences  
between Sample Means

ENDF/B-V: 0.016  
 ENDF/B-VI.2: 0.020  
 ENDF/B-VI.3: 0.019

Figure 2. Pin Power Distribution in Central Assembly of Core C.

Table 2. MCNP Results for Infinite-Lattice Configurations.

Configuration	Parameter	ENDF/B-V	ENDF/B-VI.2	ENDF/B-VI.3
A	$k_{\infty}$	$1.0582 \pm 0.0003$	$1.0562 \pm 0.0003$	$1.0560 \pm 0.0003$
	$\delta_{25}$	$0.1324 \pm 0.0001$	$0.1309 \pm 0.0001$	$0.1297 \pm 0.0001$
	$\delta_{28}$	$0.0647 \pm 0.0001$	$0.0649 \pm 0.0001$	$0.0649 \pm 0.0001$
	$\rho_{25}$	$0.3475 \pm 0.0003$	$0.3374 \pm 0.0003$	$0.3619 \pm 0.0004$
	$\rho_{28}$	$2.2774 \pm 0.0023$	$2.2980 \pm 0.0024$	$0.2923 \pm 0.0024$
	CR*	$0.4676 \pm 0.0003$	$0.4726 \pm 0.0003$	$0.4710 \pm 0.0004$
B	$k_{\infty}$	$1.0486 \pm 0.0003$	$1.0471 \pm 0.0003$	$1.0466 \pm 0.0003$
	$\delta_{25}$	$0.1176 \pm 0.0001$	$0.1163 \pm 0.0001$	$0.1153 \pm 0.0001$
	$\delta_{28}$	$0.0600 \pm 0.0001$	$0.0601 \pm 0.0001$	$0.0601 \pm 0.0001$
	$\rho_{25}$	$0.3089 \pm 0.0003$	$0.2999 \pm 0.0003$	$0.3211 \pm 0.0003$
	$\rho_{28}$	$2.0282 \pm 0.0021$	$2.0494 \pm 0.0023$	$2.0448 \pm 0.0023$
	CR*	$0.4380 \pm 0.0003$	$0.4427 \pm 0.0003$	$0.4414 \pm 0.0003$
C	$k_{\infty}$	$0.9860 \pm 0.0003$	$0.9850 \pm 0.0003$	$0.9842 \pm 0.0003$
	$\delta_{25}$	$0.1307 \pm 0.0001$	$0.1293 \pm 0.0001$	$0.1282 \pm 0.0001$
	$\delta_{28}$	$0.0656 \pm 0.0001$	$0.0656 \pm 0.0001$	$0.0658 \pm 0.0001$
	$\rho_{25}$	$0.3442 \pm 0.0004$	$0.3339 \pm 0.0004$	$0.3585 \pm 0.0004$
	$\rho_{28}$	$2.2729 \pm 0.0025$	$2.2874 \pm 0.0025$	$2.2859 \pm 0.0025$
	CR*	$0.4670 \pm 0.0004$	$0.4710 \pm 0.0004$	$0.4700 \pm 0.0004$
	PAF**	$0.1393 \pm 0.0002$	$0.1387 \pm 0.0002$	$0.1389 \pm 0.0002$

\* Conversion Ratio

\*\* Pyrex Absorption Fraction

Water Hole	1.051 ± 0.004	0.998 ± 0.003	0.977 ± 0.003	0.970 ± 0.003	0.979 ± 0.003	0.953 ± 0.003	0.946 ± 0.003
	1.060 ± 0.004	0.998 ± 0.003	0.975 ± 0.003	0.971 ± 0.003	0.979 ± 0.003	0.961 ± 0.003	0.948 ± 0.003
	1.054 ± 0.004	0.996 ± 0.003	0.972 ± 0.003	0.971 ± 0.003	0.978 ± 0.003	0.959 ± 0.003	0.944 ± 0.003
	1.020 ± 0.003	1.051 ± 0.002	1.003 ± 0.002	0.999 ± 0.002	1.040 ± 0.002	0.980 ± 0.002	0.945 ± 0.002
	1.028 ± 0.003	1.049 ± 0.002	0.998 ± 0.002	0.998 ± 0.002	1.041 ± 0.002	0.983 ± 0.002	0.950 ± 0.002
	1.022 ± 0.003	1.052 ± 0.002	0.998 ± 0.002	1.001 ± 0.002	1.040 ± 0.002	0.980 ± 0.002	0.951 ± 0.002
		Water Hole	1.069 ± 0.002	1.076 ± 0.002	Water Hole	1.035 ± 0.002	0.962 ± 0.002
			1.070 ± 0.002	1.072 ± 0.002		1.042 ± 0.002	0.962 ± 0.002
			1.065 ± 0.002	1.079 ± 0.002		1.038 ± 0.002	0.967 ± 0.002
			1.047 ± 0.003	1.090 ± 0.002	1.080 ± 0.002	0.992 ± 0.002	0.962 ± 0.002
			1.048 ± 0.003	1.095 ± 0.002	1.081 ± 0.002	0.994 ± 0.002	0.962 ± 0.002
			1.050 ± 0.003	1.094 ± 0.002	1.081 ± 0.002	0.993 ± 0.002	0.967 ± 0.002
				Water Hole	1.060 ± 0.002	0.974 ± 0.002	0.947 ± 0.002
					1.053 ± 0.002	0.971 ± 0.002	0.950 ± 0.002
					1.058 ± 0.002	0.969 ± 0.002	0.945 ± 0.002
					0.990 ± 0.003	0.952 ± 0.002	0.944 ± 0.002
					0.987 ± 0.003	0.949 ± 0.002	0.941 ± 0.002
					0.990 ± 0.003	0.954 ± 0.002	0.942 ± 0.002
						0.943 ± 0.003	0.938 ± 0.002
						0.939 ± 0.003	0.936 ± 0.002
						0.941 ± 0.003	0.934 ± 0.002
						ENDF/B-V	0.939 ± 0.003
						ENDF/B-VI.2	0.932 ± 0.003
						ENDF/B-VI.3	0.937 ± 0.003

Figure 3. Assembly Pin Power Distribution for Infinite Lattice Configuration B.

Water Hole	1.135 ± 0.004	1.018 ± 0.003	1.007 ± 0.003	1.002 ± 0.003	0.999 ± 0.003	1.039 ± 0.003	1.067 ± 0.004
	1.131 ± 0.004	1.015 ± 0.003	1.004 ± 0.003	1.001 ± 0.003	1.001 ± 0.003	1.036 ± 0.003	1.066 ± 0.004
	1.137 ± 0.004	1.016 ± 0.003	1.009 ± 0.003	1.000 ± 0.003	1.003 ± 0.003	1.037 ± 0.003	1.059 ± 0.004
1.037 ± 0.003	0.932 ± 0.002	0.968 ± 0.002	0.963 ± 0.002	0.932 ± 0.002	0.932 ± 0.002	1.006 ± 0.002	1.056 ± 0.003
1.038 ± 0.003	0.932 ± 0.002	0.969 ± 0.002	0.963 ± 0.002	0.932 ± 0.002	0.932 ± 0.002	1.010 ± 0.002	1.058 ± 0.003
1.037 ± 0.003	0.930 ± 0.002	0.968 ± 0.002	0.964 ± 0.002	0.930 ± 0.002	0.930 ± 0.002	1.005 ± 0.002	1.054 ± 0.003
	Pyrex Rod	0.874 ± 0.002	0.874 ± 0.002	0.868 ± 0.002	Pyrex Rod	0.948 ± 0.002	1.047 ± 0.002
		0.874 ± 0.002	0.874 ± 0.002	0.869 ± 0.002		0.944 ± 0.002	1.049 ± 0.002
		0.876 ± 0.002	0.876 ± 0.002	0.870 ± 0.002		0.943 ± 0.002	1.043 ± 0.002
		0.893 ± 0.003	0.893 ± 0.003	0.849 ± 0.002	0.882 ± 0.002	1.007 ± 0.002	1.073 ± 0.003
		0.895 ± 0.003	0.895 ± 0.003	0.851 ± 0.002	0.883 ± 0.002	1.008 ± 0.002	1.063 ± 0.003
		0.891 ± 0.003	0.891 ± 0.003	0.848 ± 0.002	0.881 ± 0.002	1.006 ± 0.002	1.068 ± 0.003
	Pyrex Rod			0.925 ± 0.002	0.925 ± 0.002	1.043 ± 0.002	1.086 ± 0.003
				0.923 ± 0.002	0.923 ± 0.002	1.046 ± 0.002	1.087 ± 0.003
				0.924 ± 0.002	0.924 ± 0.002	1.047 ± 0.002	1.089 ± 0.003
				1.022 ± 0.003	1.022 ± 0.003	1.081 ± 0.002	1.105 ± 0.003
				1.022 ± 0.003	1.022 ± 0.003	1.086 ± 0.002	1.105 ± 0.003
				1.020 ± 0.003	1.020 ± 0.003	1.086 ± 0.002	1.113 ± 0.003
						1.113 ± 0.003	1.125 ± 0.003
						1.109 ± 0.003	1.128 ± 0.003
						1.117 ± 0.003	1.129 ± 0.003
						ENDF/B-V	1.135 ± 0.004
						ENDF/B-VI.2	1.137 ± 0.004
						ENDF/B-VI.3	1.138 ± 0.004

Figure 4. Assembly Pin Power Distribution for Infinite Lattice Configuration C.

### RMS Differences between Libraries

Case	ENDF/B-V vs ENDF/B-VI.2	ENDF/B-V vs ENDF/B-VI.3	ENDF/B-VI.2 vs ENDF/B-VI.3
Core B	0.016	0.011	0.015
Core C	0.016	0.017	0.018
Infinite Lattice B	0.004	0.003	0.004
Infinite Lattice C	0.003	0.003	0.003